

MR853-748
Serial Number: 10/724,551
Reply to Office Action dated 1 July 2005

IN THE CLAIMS:

This Listing of Claims will replace all prior versions, and listings, of claims in the subject Patent Application:

Listing of Claims:

1-10. (Canceled).

11. (Currently Amended) An non-periodic echelle structure for use in an optical device comprising:

a grating surface disposed between input and output apertures, the grating surface including a plurality of contiguous reflective facet portions selectively disposed in a non-constant period arrangement to achieve any arbitrary desired define a predetermined narrow-band temporal optical transfer function H(v) between the device's single-mode input and output apertures, where v represents frequency in Hz and H(v) represents is a complex function having an amplitude A(v) and a phase Θ(v), the transfer function being not achievable by means of a periodic echelle structure;

the non-periodic echelle structure comprising a plurality respective facets of at least a pair of contiguous reflective facets, portions being unequally spaced along any dimension in spacing[,] and of unequal width dimensions.

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12. (Currently Amended) An optical device for realizing an arbitrary narrow-band temporal optical transfer function; the device comprising:

entrance and exit apertures each operable to which are spatially single-mode filter an optical field incident thereon over a the prescribed wavelength range of operation;

an non-periodic echelle structure disposed between the entrance and exit apertures, the echelle structure having a grating surface including a plurality of contiguous reflective facet portions selectively disposed in a non-constant period arrangement, respective facets of at least a pair of contiguous reflective facet portions being unequally spaced along any dimension in spacing[[],] and of an unequal width dimensions; and

a means of collimating optical outputs of the single-mode entrance and exit apertures such that components of an the input beam, resulting from the collimation of the single-mode entrance aperture, is incident upon a each facet of the grating surface of the non-periodic echelle structure at a common angle of incidence, and components of an the output beam reflected by the grating surface toward, resulting from the collimation of the single-mode exit aperture, is also incident upon each facet of the non-periodic echelle structure being directed at a common angle relative to a of incidence, input and output beams intersecting over an area encompassing all the reflective facets of the grating surface said non-periodic echelle structure.

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13. (Currently Amended) A method of fabricating an non-periodic echelle structure having a grating surface including a plurality of reflective facet portions selectively disposed in a non-constant period arrangement, respective facets of at least a pair of reflective facet portions being unequal in spacing along any dimension, and of an unequal width dimensions, for use in an optical system having input and output apertures; the method comprising the steps of:

- a) selecting an appropriate sampling interval of T seconds, where T is not longer than one-half the reciprocal of a frequency range, in Hz, over which a predetermined desired narrow-band temporal optical transfer function H(v) is to be uniquely specified, where v represents frequency in Hz and H(v) represents a complex function having an amplitude A(v) and a phase Θ(v);
- b) selecting a number M of echelle facets to be illuminated by an input optical beam, based upon the chosen sampling interval T and a the minimum resolvable spectral feature W, in Hz, present in either the amplitude A(v) or the phase θ(v), where M ≥ $\frac{1}{WT}$ rounded up to the nearest integer;
- c) specifying a the frequency vc, in Hz, about which a characteristic curve for H(v) is approximately centered;
- d) determining a the vector \vec{h} of complex impulse response

coefficients, each defined by the m'th coefficient, $h_m = \int_{vc - \frac{1}{2T}}^{vc + \frac{1}{2T}} H(v) e^{j2\pi mv} dv$, having an

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amplitude a_m and a phase φ_m , where $j = \sqrt{-1}$ is the imaginary unit, where m represents a counting index for the complex impulse response coefficients and $0 \leq m \leq M - 1$;

e) normalizing the complex impulse response coefficient amplitudes, a_m by multiplying each by a common factor K , such that $\sum_{m=0}^{M-1} K \cdot a_m = 1$;

f) starting at one edge of the input beam, $x=0$, selecting a the transverse width w_0 of a first illuminated facet, corresponding to $m=0$, such that the fraction of the input beam energy reflected by one said facet corresponds precisely to Ka_0 , whereupon said facet is located in a the transverse position between $x=0$ and $x=w_0$

g) selecting a the transverse width w_1 of the next illuminated facet in the grating surface array, corresponding to $m=1$, such that the fraction of the input beam signal energy reflected by said next illuminated facet corresponds precisely to Ka_1 , whereupon said next illuminated facet is located in a the transverse position between $x=w_0$ and $x=w_0+w_1$;

h) iterating step g) $M-2$ times, to find respective the transverse widths and transverse positions for the remaining $M-2$ illuminated facets;

i) setting the precise longitudinal position, along the direction of propagation of the input beam, of the center of the m^{th} m^{th} illuminated facet, such that a the relative delay, compared to a predetermined any arbitrary time reference,

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experienced by an optical ray incident upon said illuminated facet and collected at the exit aperture is defined by $\Delta t_m = mT + \varphi_m / (2\pi c)$.

14. (Currently Amended) The method of fabricating the ~~non-periodic~~ echelle structure recited in claim 13, ~~generalized to geometries other than collimated the input and output beams are collimated.~~

15. (Currently Amended) The ~~non-periodic~~ echelle structure recited in claim 11 wherein said structure is replicated from a master.

16. (Currently Amended) The ~~non-periodic~~ echelle structure recited in claim 11 wherein each said facet being illuminated is coated for increased reflectivity.

17. (Previously Presented) The method recited in claim 14 wherein at least one of said entrance and exit apertures comprises a single-mode optical fiber.

18. (Currently Amended) The method recited in claim 14 further comprising the steps of confining said optical beam in at least one direction with a single mode slab waveguide and wherein said ~~non-periodic~~ echelle structure is formed in an edge of said slab waveguide.